

# Interlaminar fracture tests: why we love UD specimens, why we hate multidirectional ones, and can this change?

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# Why even ask?

Structural applications → **MD** laminates

But

Interlaminar fracture standards → **UD** specimens

Why?

Is this conservative? → Not obvious

Is toughness the same? → Not obvious

Is it that we like UD specimens more?  
If so, why?

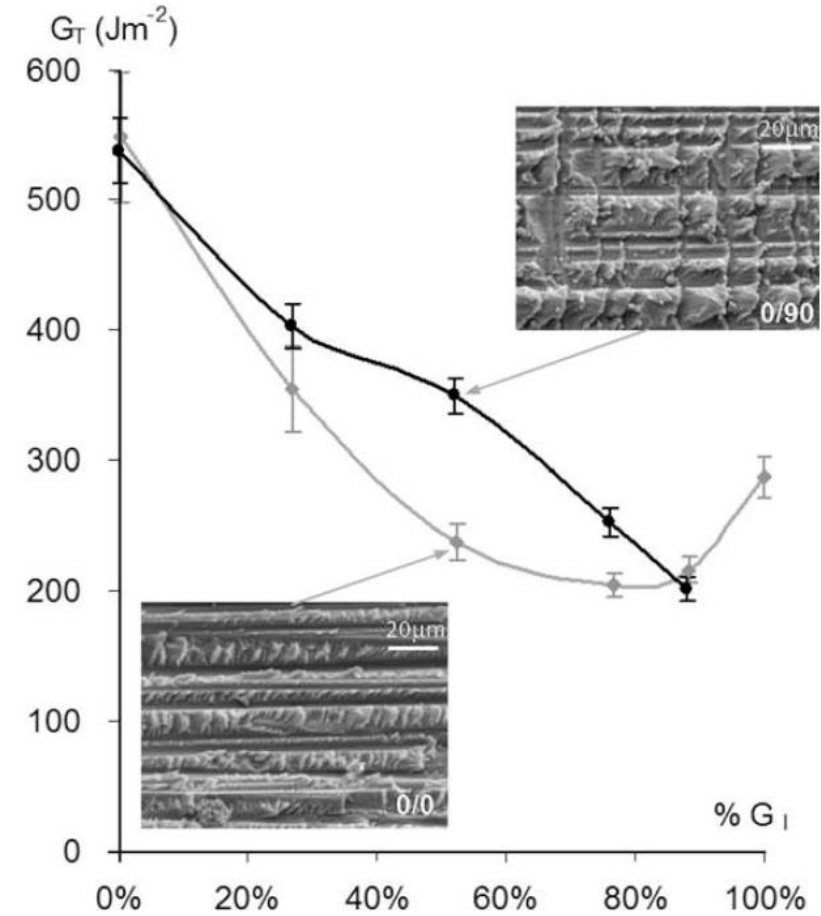
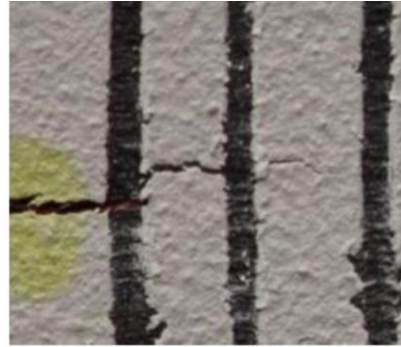


Fig. 5. Failure loci for 0/0 and 0/90 ply interfaces for T800/924.

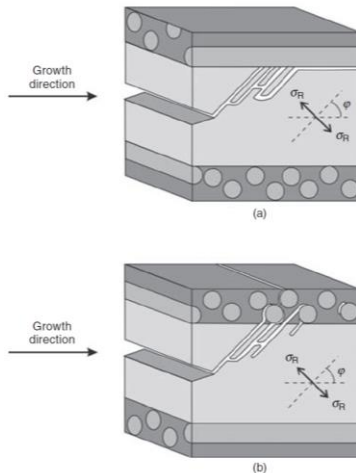
[Greenhalgh et al. 2009](#)

# Why we love UD specimens, why we hate multidirectional ones?

## 1. Delamination migration



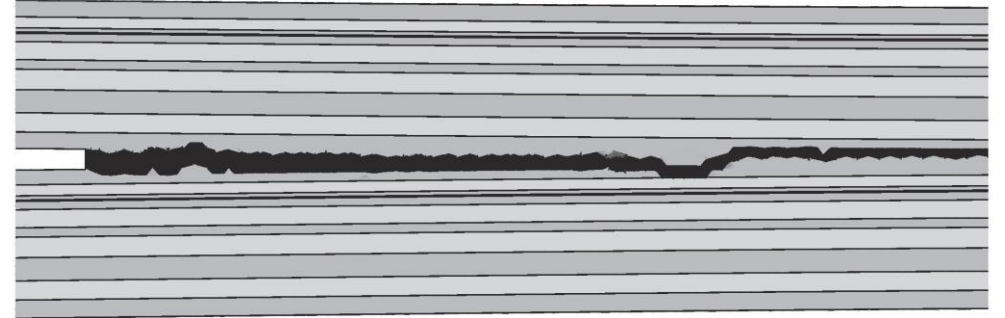
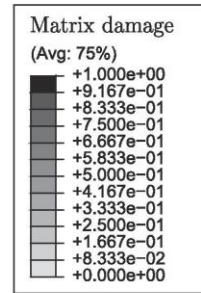
[Santos et al., 2023](#)



[Greenhalgh, 2009](#)

## UD specimens: migration does not occur

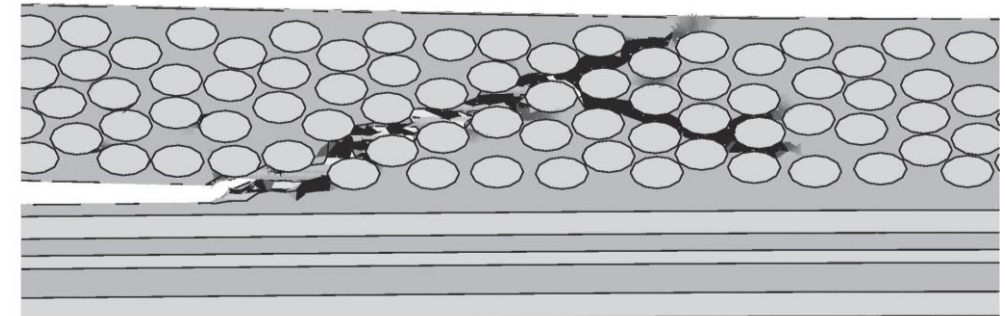
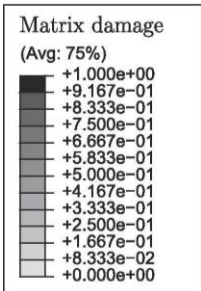
[Varandas et al., 2019](#)



(a)  $0^\circ/0^\circ$  UC.

## MD specimens: migration can occur

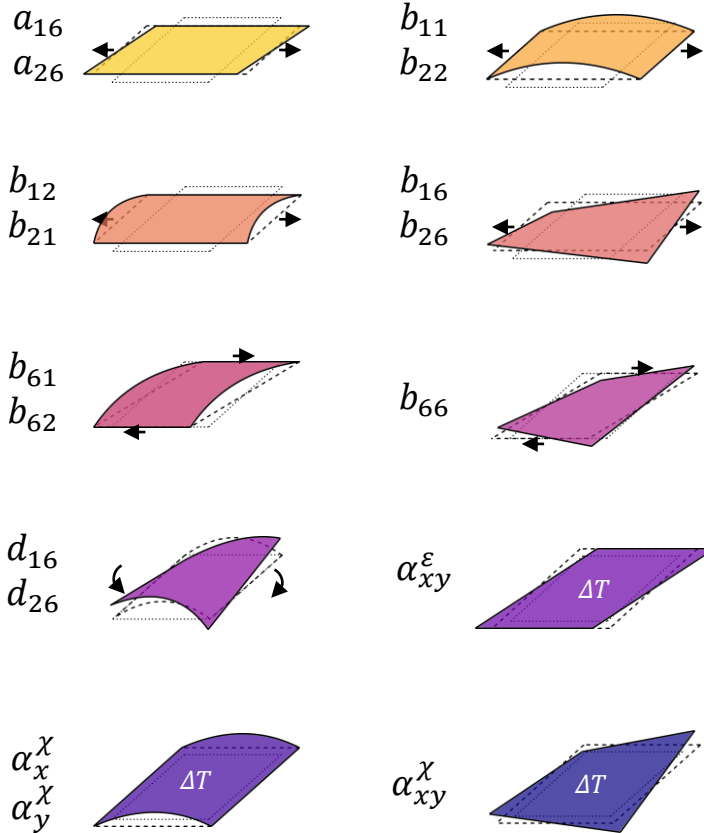
[Varandas et al., 2019](#)



(b)  $45^\circ/0^\circ$  UC.

# Why we love UD specimens, why we hate multidirectional ones?

## 2. Thermoelastic couplings



$$B_t = \left| \frac{D_{16}}{D_{11}} \right|$$

## UD laminate

$$\begin{Bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \varepsilon_{xy}^0 \\ \chi_x \\ \chi_y \\ \chi_{xy} \end{Bmatrix} = \begin{bmatrix} a_{11} & a_{12} & 0 & 0 & 0 & 0 \\ a_{12} & a_{22} & 0 & 0 & 0 & 0 \\ 0 & 0 & a_{66} & 0 & 0 & 0 \\ 0 & 0 & 0 & d_{11} & d_{12} & 0 \\ 0 & 0 & 0 & d_{12} & d_{22} & 0 \\ 0 & 0 & 0 & 0 & 0 & d_{66} \end{bmatrix} \begin{Bmatrix} N_x \\ N_y \\ N_{xy} \\ M_x \\ M_y \\ M_{xy} \end{Bmatrix} + \Delta T \begin{Bmatrix} \alpha_x^\varepsilon \\ \alpha_y^\varepsilon \\ 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

Inverse constitutive law (CLPT)

## MD laminate

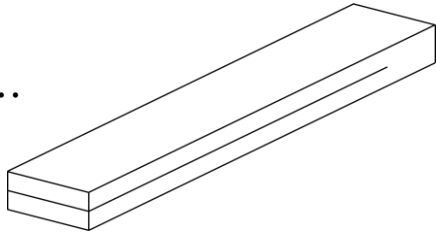
$$\begin{Bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \varepsilon_{xy}^0 \\ \chi_x \\ \chi_y \\ \chi_{xy} \end{Bmatrix} = \begin{bmatrix} a_{11} & a_{12} & a_{16} & b_{11} & b_{12} & b_{16} \\ a_{12} & a_{22} & a_{26} & b_{21} & b_{22} & b_{26} \\ a_{16} & a_{26} & a_{66} & b_{61} & b_{62} & b_{66} \\ b_{11} & b_{21} & b_{61} & d_{11} & d_{12} & d_{16} \\ b_{12} & b_{22} & b_{62} & d_{12} & d_{22} & d_{26} \\ b_{16} & b_{26} & b_{66} & d_{16} & d_{26} & d_{66} \end{bmatrix} \begin{Bmatrix} N_x \\ N_y \\ N_{xy} \\ M_x \\ M_y \\ M_{xy} \end{Bmatrix} + \Delta T \begin{Bmatrix} \alpha_x^\varepsilon \\ \alpha_y^\varepsilon \\ \alpha_{xy}^\varepsilon \\ \alpha_x^\chi \\ \alpha_y^\chi \\ \alpha_{xy}^\chi \end{Bmatrix}$$

Inverse constitutive law (CLPT)

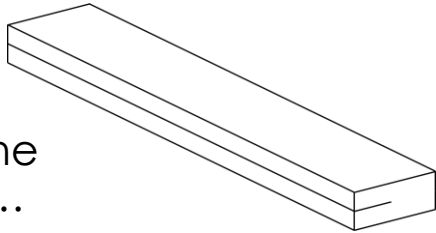
# Why we love UD specimens, why we hate multidirectional ones?

## 3. Finite width effect

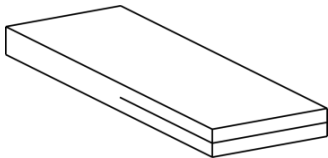
Plane stress ...



... plane strain ...

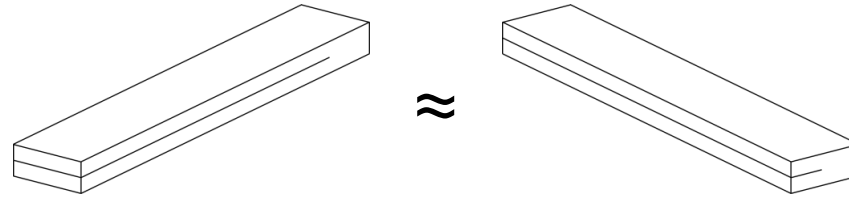


... or ?



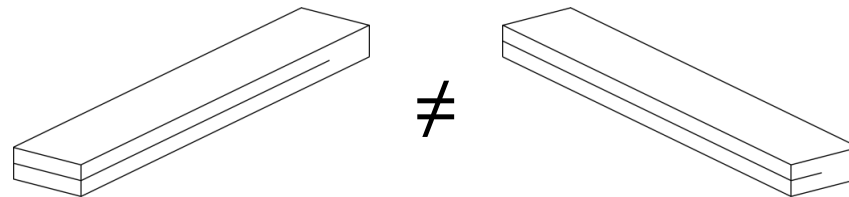
$$D_c = \frac{D_{12}^2}{D_{11}D_{22}}$$

## UD specimens



- Low  $D_c$
- Negligible effect

## MD specimens

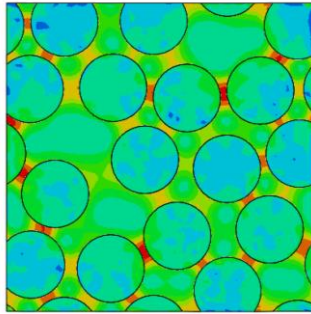


- Potentially high  $D_c$
- Significant effect
  - Uneven ERR at front
  - Curved front
  - Non-self-similar propagation

# Why we love UD specimens, why we hate multidirectional ones?

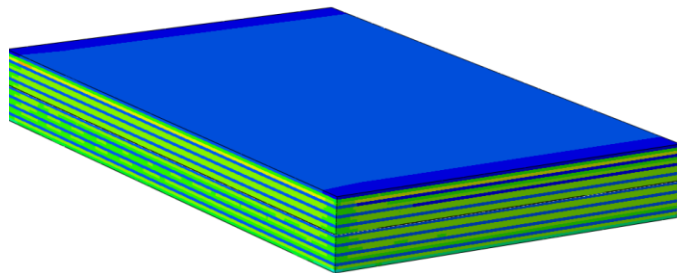
## 4. Thermal residual stresses

Micro residual stresses

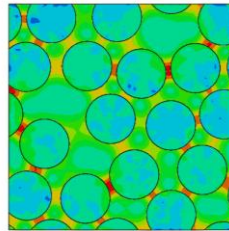


[Gonçalves et al., 2022](#)

Ply-level residual stresses

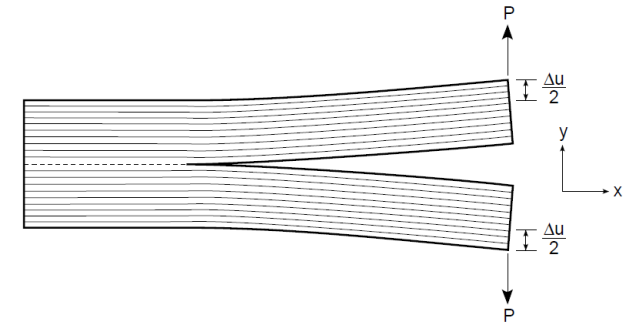


## UD specimens



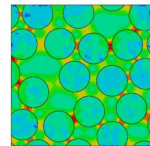
Micro-residual stresses only

[Nairn, 1997](#)

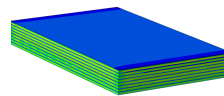


Micro-residual stresses do not release energy during delamination propagation

## MD specimens



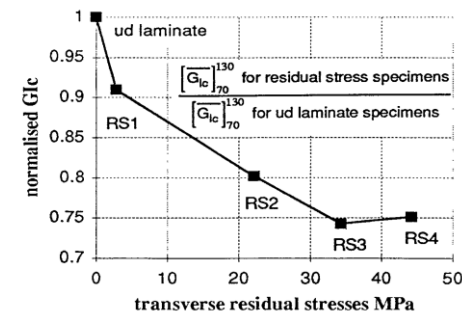
+



Both micro and ply-level residual stresses

[Nairn, 2000](#): suggests double symmetric layups

[Robinson et al., 1996](#)



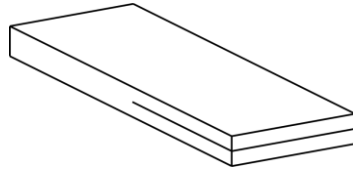
[Sebaey et al., 2011](#): Ply-level stresses facilitate migration

[Gonçalves et al., 2023](#): Micro & ply-level stresses reduce effective strength

# Can this change?

## Fully-Uncoupled Multidirectional (FUMD) specimens, concept

[Garulli et al., 2019](#)



$$\begin{Bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \varepsilon_{xy}^0 \\ \chi_x \\ \chi_y \\ \chi_{xy} \end{Bmatrix} = \begin{bmatrix} a_{11} & a_{12} & 0 & 0 & 0 & 0 \\ a_{12} & a_{22} & 0 & 0 & 0 & 0 \\ 0 & 0 & a_{66} & 0 & 0 & 0 \\ 0 & 0 & 0 & d_{11} & d_{12} & 0 \\ 0 & 0 & 0 & d_{12} & d_{22} & 0 \\ 0 & 0 & 0 & 0 & 0 & d_{66} \end{bmatrix} \begin{Bmatrix} N_x \\ N_y \\ N_{xy} \\ M_x \\ M_y \\ M_{xy} \end{Bmatrix} + \Delta T \begin{Bmatrix} \alpha_x^\varepsilon \\ \alpha_y^\varepsilon \\ 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

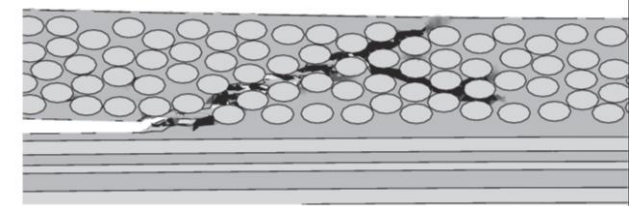
Set of MD specimens with UD-like thermoelastic behaviour

- No couplings (in arms or uncracked region)
- Free orientations choice
- Arbitrary interface

## What may be missing?

Migration:

Can we avoid it in mode I tests?



[Varandas et al., 2019](#)

## FUMD preliminary experimental results



UD



FUMD 0//30



FUMD 0//0



FUMD 0//45

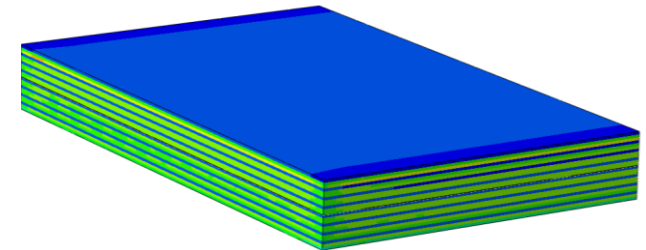


FUMD 0//15

[Garulli et al., 2020](#)

Residual stresses:

Can we fully understand their effects?





# Conclusions

There are many (reasonable) reasons to love UD specimens

- As easy and as convenient as it gets
- Allow reasonable structural predictions (surprisingly)

There are (still) a few reasons to hate MD specimens:

- More complex behaviour
- Unsolved issues

Can this change?

- Potentially, with some research effort
- If it does, it will enable us to deliberately choose whether to use UD or MD specimens!