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Multi-Objective Optimization for Fibrous Composite Reinforced by Curvilinear Fibers

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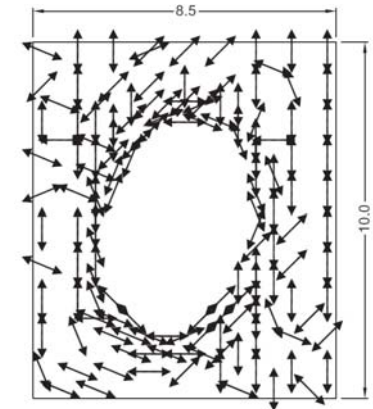
3-2. Fiber shapes (discretized) & failure indexes

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Developing manufacturing technique

- Composite with curvilinear fiber shape
- Automated tow-placement technique
- Natural materials(ex. Bone)
- Direction of HAp crystal
- Optimally distributed anisotropy by curvilinear fiber shape.

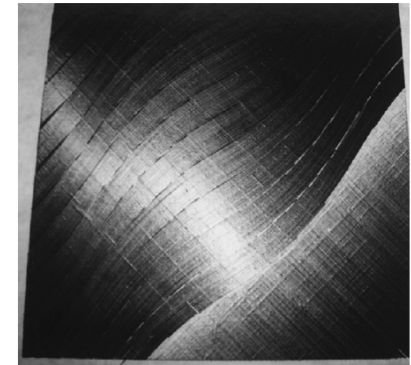
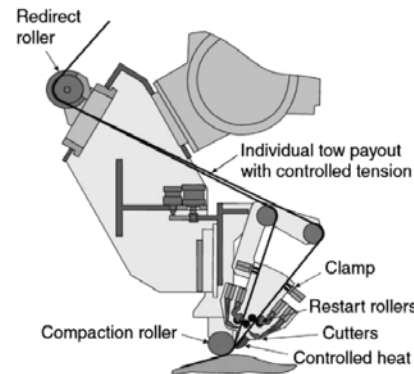


Bovine bone

Source: Giri et al. (2008)



Source: Cincinnati Machine

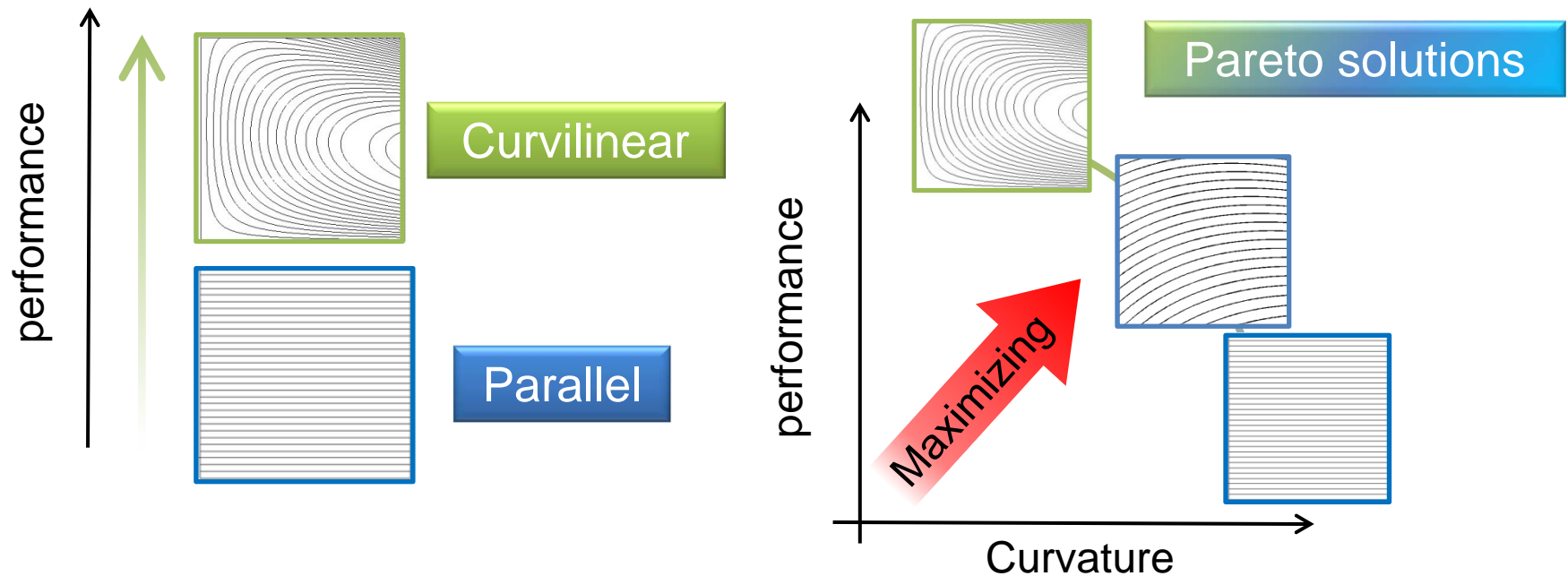


Source: Lopes et al. (2008)



In our previous study:

- Higher performance than the plate with parallel fibers.
- Large curvature & non-homogenous volume fraction.
- Trade-off relation between performance & fiber shape.
- Multi-objective optimization technique.



2-1. Fiber shape expression

The curvilinear fiber shapes are denoted by the projections of contour lines for a cubic polynomial surface $f(x, y)$.

surface:
$$f(x, y) = c_{10}x + c_{01}y + c_{20}x^2 + c_{11}xy + c_{02}y^2 + c_{30}x^3 + c_{21}x^2y + c_{12}xy^2 + c_{03}y^3$$

Example)

c_{10}	c_{01}	c_{20}	c_{11}	c_{02}	c_{30}	c_{21}	c_{12}	c_{03}
0.8	-0.8	0.2	-0.5	0.2	-1	-0.9	1	1

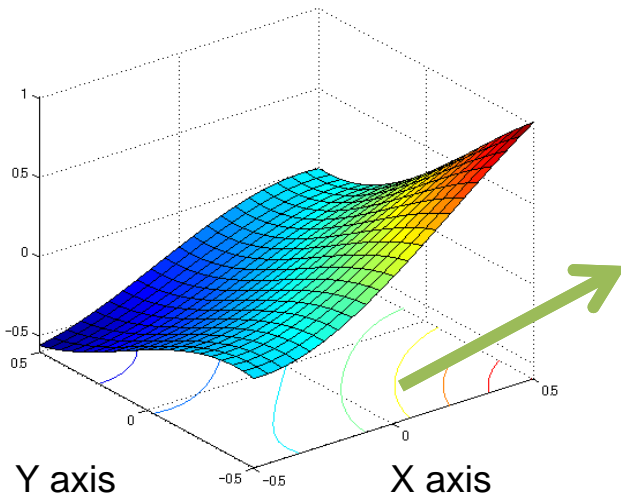


Fig. Surface & Contour lines

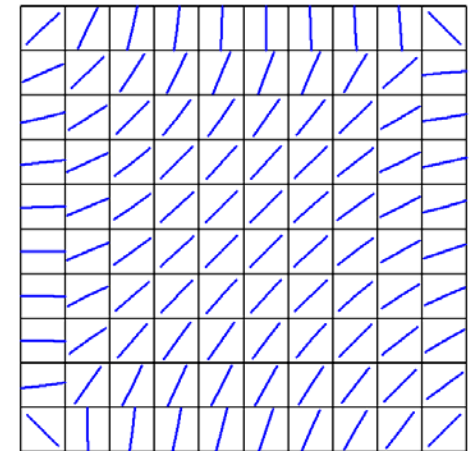
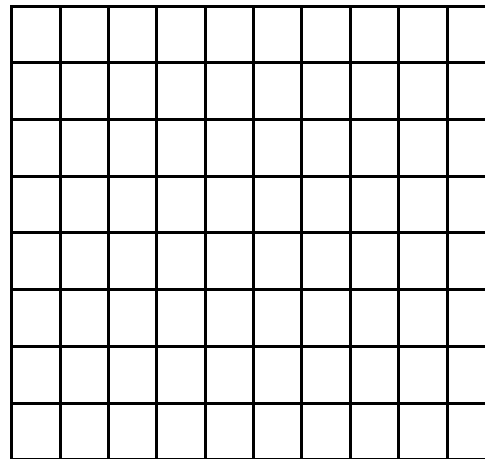


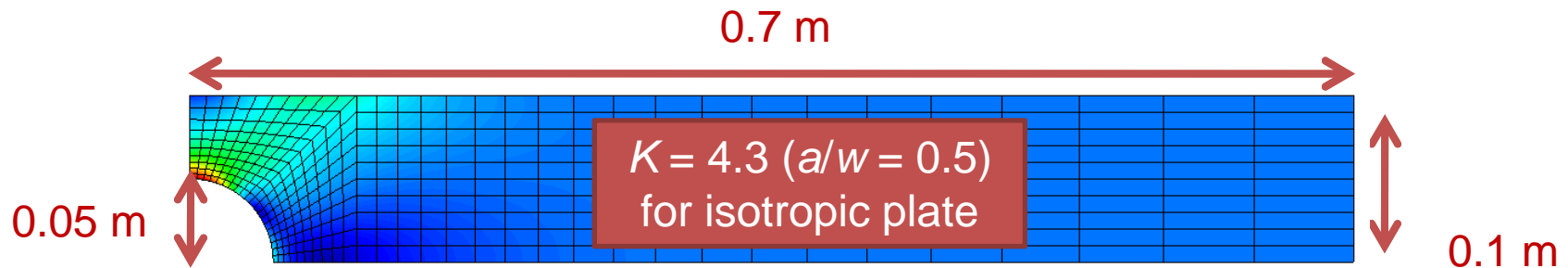
Fig. Discrete fiber shape in the FEA



2-2. Modeling of the plate with circular hole

- **Plate**: Quarter model of the plate with finite width and infinite length

$$w = 0.1 \text{ [m]}, a = 0.05 \text{ [m]}, c = 0.7 \text{ [m]}, \sigma_x = 10 \text{ [MPa]}$$



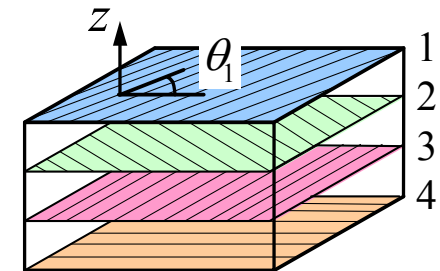
Number of elements around the hole = 200

Total number of elements = 400

- **Material**: Graphite/epoxy (CFRP)

Symmetric 8-layer angle-ply plate $[+/-/+/-]_s$

$$E_1 = 138 \text{ [GPa]}, E_2 = 8.96 \text{ [GPa]}, G_{12} = 7.1 \text{ [GPa]}, \nu_{12} = 0.30$$



Sym. $[+\theta/-\theta/+ \theta/-\theta]_s$



2-3. Objective functions

1. Maximizing in-plane strength around circular hole

➔ Minimizing Tsai-Wu failure index Φ

$$\Phi = F_1\sigma_1 + F_2\sigma_2 + F_{11}\sigma_1^2 + F_{22}\sigma_2^2 + F_{12}\sigma_1\sigma_2 + F_{66}\tau_{12}^2 \quad (\Phi \geq 1 : \text{Failure})$$

$$\left(\begin{array}{l} F_1 = (X_c - X_t)/(X_c X_t), \quad F_2 = (Y_c - Y_t)/(Y_c Y_t) \\ F_{11} = 1/(X_c X_t), \quad F_{22} = 1/(Y_c Y_t), \quad F_{12} = 1/(X_c X_t Y_c Y_t)^{1/2} \\ F_{66} = 1/S^2 \end{array} \quad \begin{array}{l} X_t = X_c = 144800 \text{ N/cm}^2, \\ Y_t = 20685 \text{ N/cm}^2, \quad Y_c = 5171 \text{ N/cm}^2, \\ S = 9008 \text{ N/cm}^2 \end{array} \right)$$

2. Improving practicality of curvilinear fiber shape

➔ Minimizing average curvature \bar{K}

$$\bar{K} = \frac{1}{n_e} \sum_{k=1}^{n_e} \frac{1}{\left(f_x^{(k)2} + f_y^{(k)2} \right)^{3/2}} \begin{bmatrix} -f_y^{(k)} & f_x^{(k)} \end{bmatrix} \begin{bmatrix} f_{xx}^{(k)} & f_{xy}^{(k)} \\ f_{xy}^{(k)} & f_{yy}^{(k)} \end{bmatrix} \begin{bmatrix} -f_y^{(k)} \\ f_x^{(k)} \end{bmatrix}$$

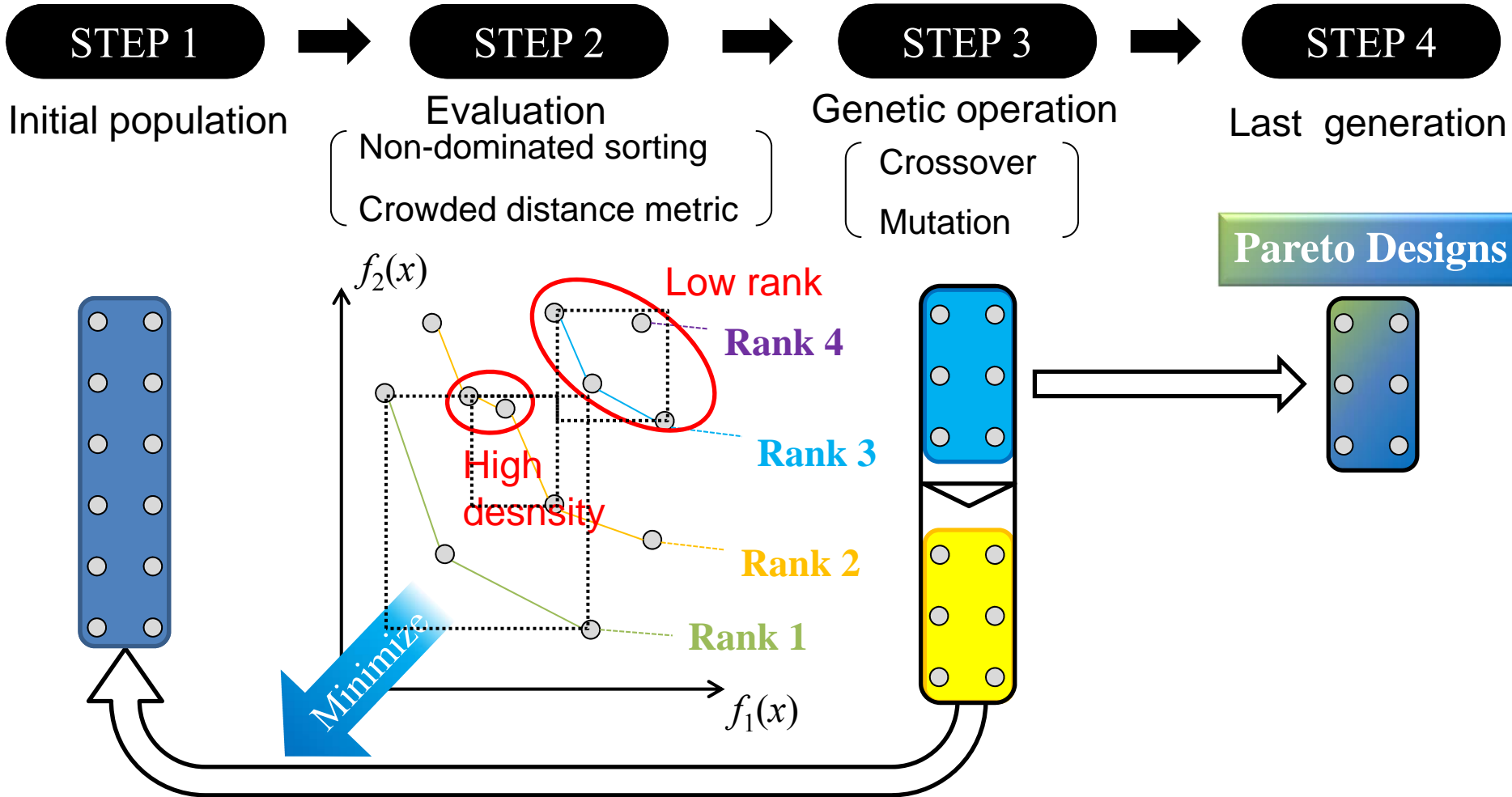
n_e : number of element, $f_*^{(k)}$: partial difference in the k th element



2-4. Multi-objective optimization technique

Improved non-dominated sorting genetic algorithm (NSGA-II)

(Deb et. al., 2002)



2-5. Formulation of Multi-objective optimization

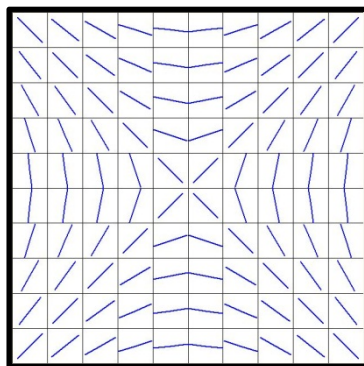
Minimizing: $(\Phi)_k$ ($k = 1, 2$) and $(\bar{\kappa})_k$ ($k = 1$)

Design variables: c_{ij} ($i, j = 0, 1, 2, 3$)

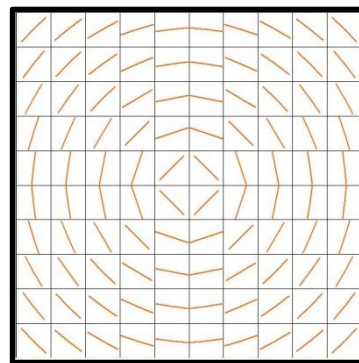
Subject to: $-2.0 \leq c_{ij} \leq 2.0$ ($\Delta c_{ij} = 0.1$) ($i, j = 0, 1, 2, \text{ and } 3$)

$$c_{10} = c_{01} = c_{11} = c_{12} = c_{21} = 0$$

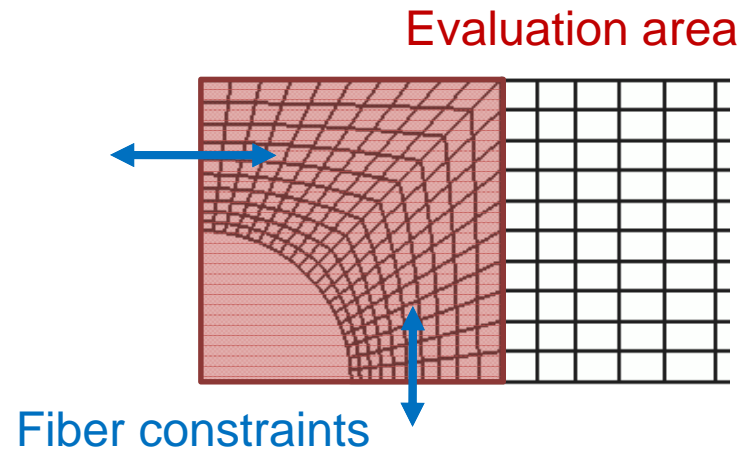
- Plates are limited to the symmetric 8 layer angle-ply plate $[+/-/+/-]_s$
- Evaluation area, $0 \leq x, y \leq 0.1$
- Number of generation: 400, Number of population: 400



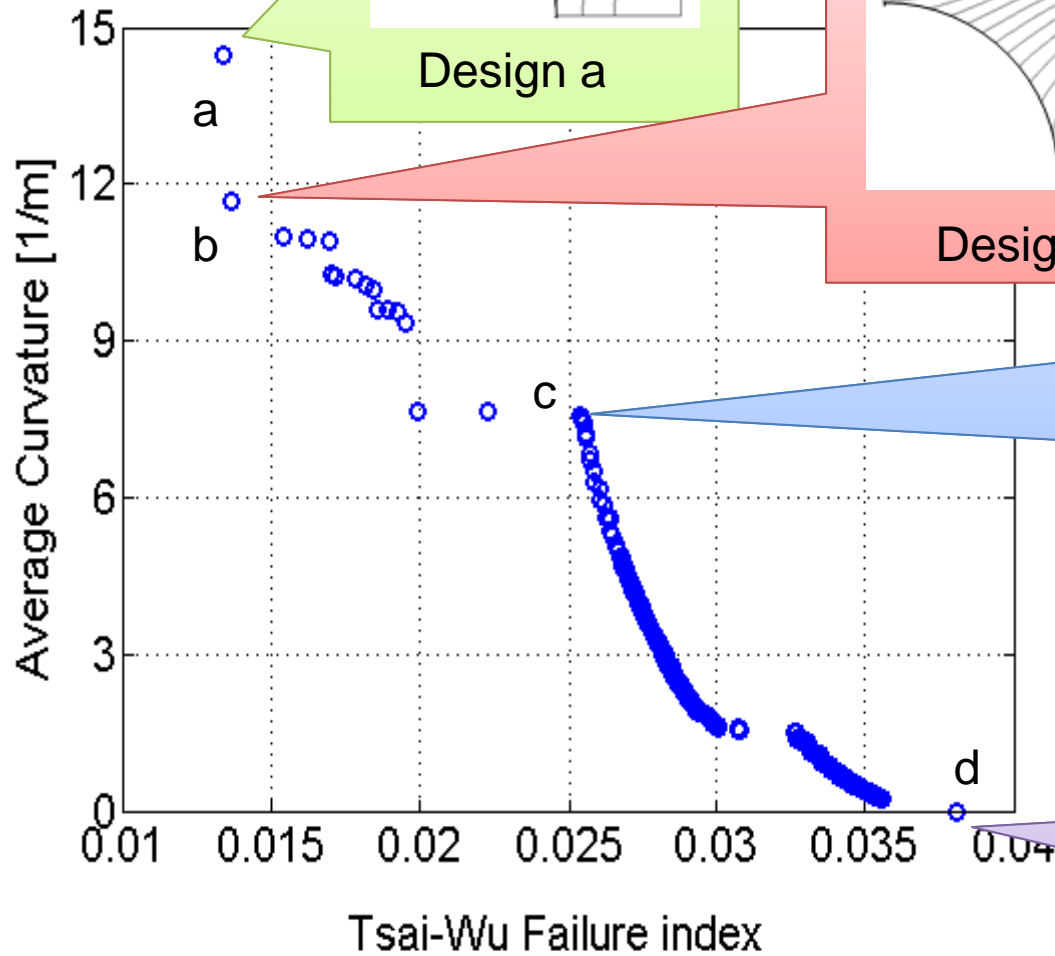
+ layer



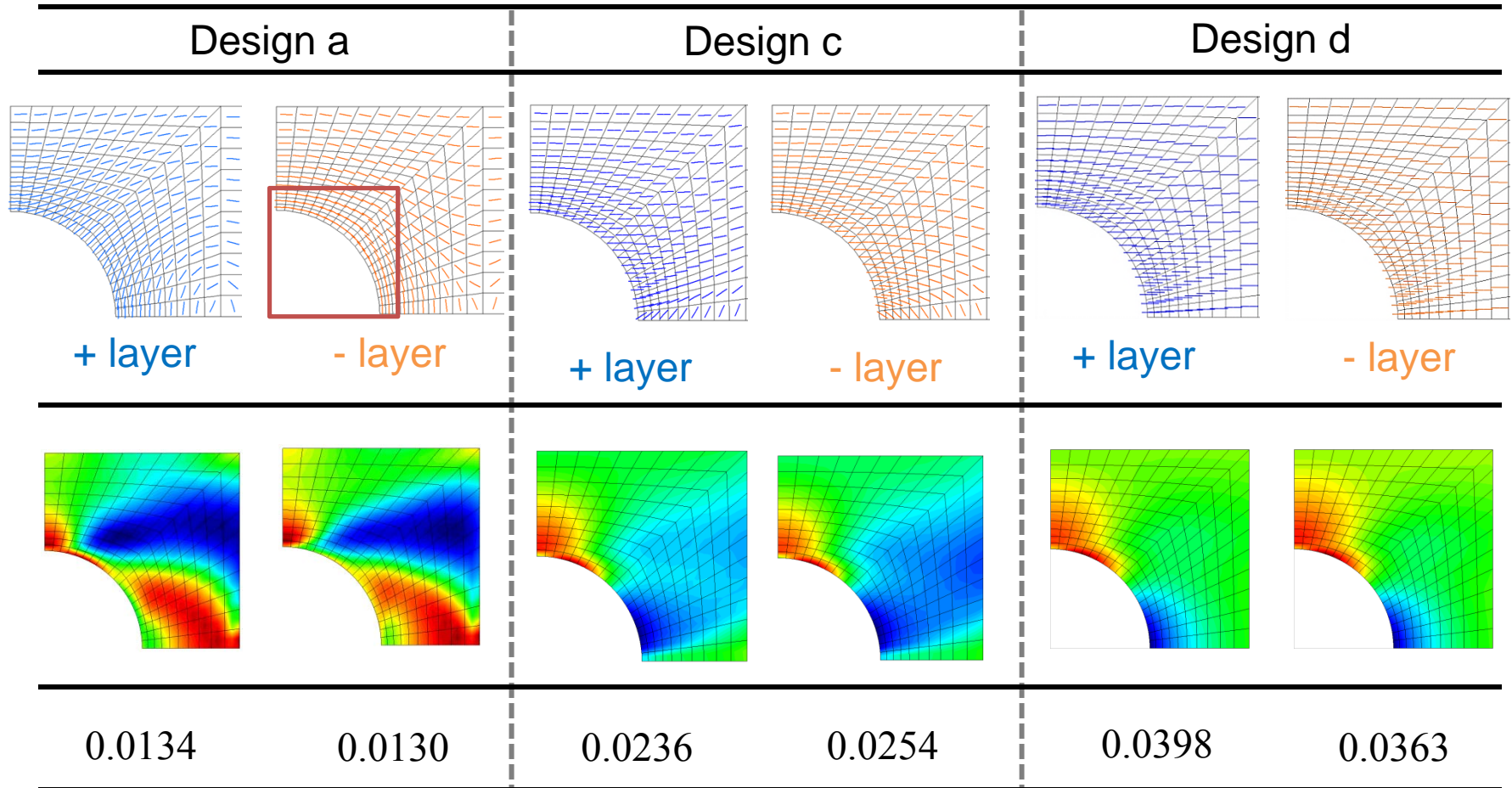
- layer



3-1. Pareto front

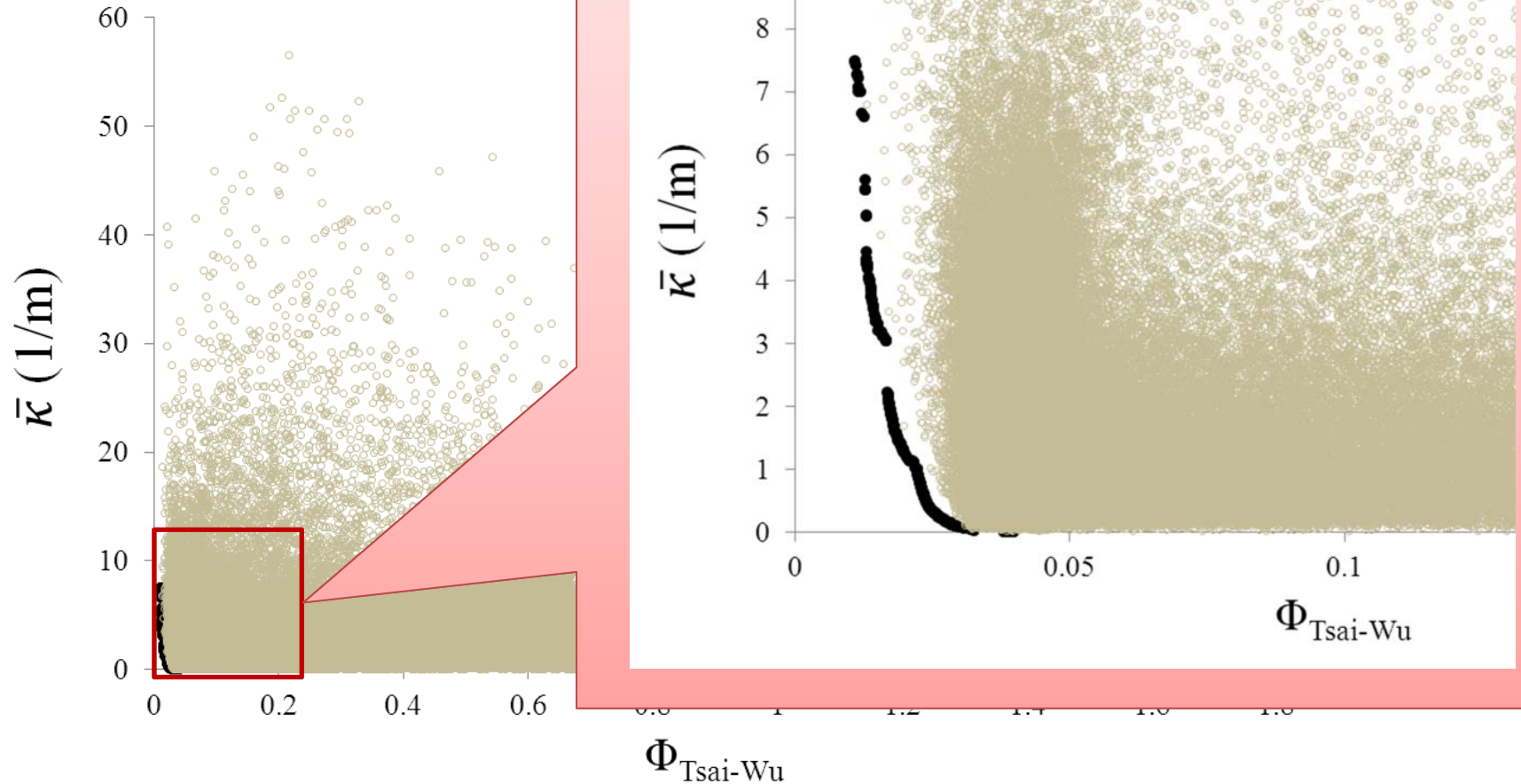


3-2. Fiber shapes (discretized) & failure indexes



3-3. Comparison with random search

- 200,000 times random search



Summary:

- The present study proposed a multi-objective optimization method to maximize the in-plane strength and minimizing production cost for the fibrous composite plate with curvilinear fibers.
- Two conflicting objectives, the in-plane strength and production cost, are represented by the Tsai-Wu failure index and average curvature, respectively.

Conclusions:

- The numerical results showed that the present optimization method resulted in the widely distributed Pareto-optimum front ranging from parallel fibers to largely curved fibers.
- Obtained solutions had higher in-plane strength than the plate with the highest strength within the parallel fiber plate. This demonstrates an advantage of curvilinear fibers in terms of in-plane strength.
- Curvilinear fiber shape shows similarity with the natural compound like bovine bone, and this established the validity of the present results.

